Introduction

The proposed development site is a parcel of land comprising the former Harthill Depot, Beechley House, Calder Kids, Riding School, Miniature Railway and Paddock area. The site is located to the north west of Calderstones Park, Liverpool. The proposed development site is approximately 5.23 Ha in overall area and is off mixed use, i.e. brownfield and greenfield. A planning application has been submitted for 39 new build properties and 12 refurbished dwellings. A summary of site areas is listed below:

Greenfield Areas = 1.0ha

Brownfield Areas = 4.23ha

Existing Site Drainage

A pre-development enquiry was submitted to United Utilities (UU) to advise on a potential discharge rate for the development. UU confirmed that an allowable discharge rate for surface water to the public sewer of 17l/s would be satisfactory. A copy of this correspondence can be found within the site's FRA. Report ref 15RED096/DS produced by Betts Associates dated August 2016.

Amey have produced a guidance note "LCC Greenfield/Brownfield Sites Surface Water Management Guidance" with regards to determining brownfield/greenfield run-off rates, which Amey have confirmed takes precedence over UU.

A drainage survey was undertaken in October 2016 to investigate the existing site drainage network for the area surrounding Beechley House and The Depot Site. It was not proven that the depot site discharged positively to the existing public sewer. A copy of the survey findings can be found within Appendix B.

Existing Flow Rates / Capacity

The results of the survey confirm that the final connection from Beechley House into the public sewer is laid a gradient such that the pipe can facilitate a flow rate of 26l/s. Therefore in order to calculate the allowable proposed discharge rate from the site 30% betterment is applied, which indicates an allowable discharge rate for the development of 18.2l/s.

United Utilities have confirmed that the capacity of the existing sewer can only facilitate a maximum discharge of surface water from the development of 17I/s therefore in this instance we must use the lower rate.

An allowable surface water discharge rate of **17l/s** shall be applied to the development.

Assessment of Site for Soakaways

A limited site investigation was undertaken during October 16. Due to the existing vegetation in the paddock area, machine access was limited and no tests were undertaken. Further tests will be undertaken post planning and vacant possession of the site is available and the area has been cleared.

Three tests were undertaken within the depot site (SA1, SA2 & SA3) these are shown on the exploratory hole location plan within Appendix C. SA1 & SA3 proved acceptable for infiltration with rates of 2.3E-05m/sec and 1.0E-05m/sec respectively. SA2 was proven to be unsuccessful as water levels failed to drain to 75% effective depth. The results are included within Appendix D.

An assessment for storage requirements using soakaways has been undertaken using Micro drainage software.

Assessment of SA1

An assessment against SA1 has been undertaken to provide volume of storage required. Plots 1-5 are located in the vicinity of SA1 and these plots have been used to assess the storage requirements. Due to the limited impermeable area a discharge rate of 2l/s is proposed. A copy of the design parameters are shown below;

	Variables				
icro	Rainfall and Runoff		Infiltration Structure		
Variables	FSR Rainfall Retum Period (years) Region England and Map M5-60 (mm) Ratio R	▼ 100 Wales ▼ 18.800 0.400	Trench Soskaway Infiltration Coefficient Base (m/hr) Infiltration Coefficient Side (m/hr) Safety Factor Porosity	0.08280 0.08280 2.0 0.30	8
Variables Results 2D Graphs 3D Graphs Structures Pollution	Cv (Summer) Cv (Winter) Impermeable Area (ha) Climate Change (%)	0.750 0.840 0.110 40	₩ With Outflow Maximum Discharge (/s)	20	
			Analyse OK	Cance	Help

Two types of soakaways have been modelling using the Microdrainage Software, a trench soakaway and a house soakaway. Results for both models are shown below;

Trench Soakaway

o nage	Results are presented in paired rows. These represent maximum and minimum storage requirements teach size of structure.									
	Width (m)	Net Vol (m³)	Length (m)	Unit Area (m²)	Ex/Fill Vol (m ³)	Half Drain (mins)				
	0.2	32.5	360.6	3.1	108.2	26				
		23.4	260.2	4.2	78.1	21				
	0.3	35.1	260.0	4.2	117.0	36				
		26.3	194.5	5.7	87.5	29				
	0.4	36.6	203.4	5.4	122.0	46				
		28.0	155.7	7.1	93.4	35				
riablee	0.6	39.3	145.6	7.6	131.0	62				
nuorea		30.4	112.8	9.8	101.5	45				
esults	1.0	42.0	93.3	11.8	139.9	86				
Graphs		32.8	72.9	15.1	109.4	58				
Graphs	1.5	43.2	64.1	17.2	144.1	107				
Graphs	_	34.4	51.0	21.6	114.8	68				
	2.0	44.1	49.0	22.4	147.0	122				
uctures	l	35.8	39.8	27.6	119.4	75				
llution										
					_					

House Soakaway

-									
age	results are presented in paired rows. These represent maximum and minimum storage requirement each size of structure.								
	Pit Size (m)	Net Vol (m³)	No Required	Unit Area (m²)	Ex/Fill Vol (m²)	Half Drain (mins)			
	1.0	36.2	121	9.1	278.3	50			
		28.6	96	11.5	220.8	38			
	1.5	38.3	57	19.3	295.0	64			
		30.7	46	23.9	238.1	47			
	2.0	39.4	33	33.3	303.6	76			
		32.3	27	40.7	248.4	53			
ablas	2.5	40.6	22	50.0	316.3	85			
aures		32.8	18	61.1	258.8	58			
sults	3.0	40.8	16	68.8	331.2	92			
araphs		33.3	13	84.6	269.1	61			
iraphs									
ctures									
lution									

A considerable length/number of soakaways is required to successfully infiltrate the plots identified above. A trench soakaway of approximately 45m long x 2m wide x 2m deep or approximately 15no 3m diameter x 2.3m deep house soakaways are required.

Soakaways are usually located approx. 5m from the back of a dwelling. On this development it is expected potential customers to construct conservatories and therefore must make an allowance for this when we design drainage systems within the plot curtilage. To avoid any potential clash the soakaways need to be located at least 9m from the back of each dwelling.

However the boundary of the site is lined by mature trees at varying heights between 12m and 25m with considerable root protection zones.

Soakaways will not be able to be constructed in the RPZ's and therefore construction of house soakaway of the required size is impractical.

Assessment of SA3

An assessment against SA3 has been undertaken to provide volume of storage required. Plots 16-21 are located in the vicinity of SA3 and these plots have been used to assess the storage requirements. Due to the limited impermeable area a discharge rate of 2l/s is proposed. A copy of the design parameters are shown below;

💜 Quick Design	: Infiltration Systems					_ 🗆 🗙
	Variables					
Micro	Rainfall and Runoff		Infiltration Structure			
Diamage	FSR Rainfall	•	Trench Soakaway	•		
	Return Period (years)	100	Infiltration Coefficient Base (m/hr)	0.03600	_	
	Region England and	Wales 👻	Infiltration Coefficient Side (m/hr)	0.03600		
	Map M5 60 (mm)	10 000	Safety Factor	2.0		
	Batio R	0.400	Porosity	0.30		
		1				
Variables	Cv (Summer)	0.750			-	
Results	Impermeable Area (ba)	0.840	Vith Outflow			
2D Graphs	Climate Change (%)	40	Maximum Discharge (1/s)	2.0		
3D Graphs		1				
Structures						
Dellution						
Follution						
			Analyse	OK	Cancel	Help
		Enter Climate	Change between -100 and 600			

As per the assessment for SA1 two types of soakaways have been modelling using the Microdrainage Software, a trench soakaway and a house soakaway. Results for both models are shown below;

Trench Soakaway

	Results									
age	Results are presented in paired rows. These represent maximum and minimum storage requirements for each size of structure.									
	Width (m)	Net Vol (m³)	Length (m)	Unit Area (m²)	Ex/Fill Vol (m ³)	Half Drain (mins)				
	0.2	44.8	498.2	2.4	149.5	57				
		33.3	369.8	3.3	110.9	43				
	0.3	48.2	357.2	3.4	160.8	79				
		36.2	268.4	4.5	120.8	56				
	0.4	49.9	277.2	4.4	166.3	99				
		37.9	210.8	5.8	126.5	67				
	0.6	52.6	194.8	6.3	175.4	131				
ables		40.0	148.2	8.2	133.4	82				
sults	1.0	55.3	122.8	9.9	184.2	179				
		42.4	94.3	12.9	141.4	100				
iraphs	1.5	57.6	85.3	14.3	192.0	219				
iraphs		44.8	66.4	18.4	149.5	115				
-	2.0	57.8	64.2	19.0	192.7	244				
ctures		45.0	50.0	24.4	150.0	122				
ution										
						. 1				

House Soakaway

	Results									
ige	Results are presented in paired rows. These represent maximum and minimum storage requirement each size of structure.									
	Pit Size (m)	Net Vol (m³)	No Required	Unit Area (m²)	Ex/Fill Vol (m ³)	Half Drain (mins)				
	1.0	49.6	166	7.3	381.8	107				
		38.5	129	9.5	296.7	71				
	1.5	52.2	78	15.6	403.7	137				
		40.1	60	20.3	310.5	84				
	2.0	52.7	44	27.7	404.8	158				
		41.7	35	34.9	322.0	93				
hlas	2.5	53.3	29	42.1	416.9	175				
Lies		42.2	23	53.0	330.6	100				
ults	3.0	54.0	20	61.0	414.0	189				
raphs		42.9	16	76.3	331.2	105				
raphs										
tures										
noit										
							or 1			

As per the assessment for SA1 a considerable length/number of soakaways is required to successfully infiltrate the plots identified above. A trench soakaway of approximately 57m long x 2m wide x 2m deep or approximately 18no 3m diameter x 2.3m deep house soakaways are required.

These plots are affected by the similar issues to those of SA1. It is considered that whilst the area in the vicinity of SA1 & SA3 is suitable to drain via infiltration and the drainage strategy is to were possible follow the SW Hierarchy as set out in the NPPF and the scheme should be in accordance with the Non-Statutory Technical standards for Sustainable Drainage systems (March 2015) the location of any such soakaway structure would be too close to building foundations, within the root protection zone, large surface area and crossing property boundary's resulting in maintenance issues, it is proposed to drain this area by a more conventional gravity system to discharge into the existing public sewer at a restricted discharge rate.

Proposed Site Drainage

The proposed development is split into three separate phases; The Depot Site (New Build), The Paddock (New Build) and Beechley House (Refurb & New Build). These phases are highlighted on the detailed site layout found in Appendix A.

The Depot Site & The Paddock will ultimately discharge into the existing public combined sewer within Harthill Road via one connection. Beechley House will drain into the existing public combined sewer within Harthill Road via an existing connection located within the Beechley House grounds. A copy of the proposed drainage layout is enclosed within Appendix C.

The Depot Site

Surface Water

The surface water drainage for The Depot Site will drain via gravity into a series of cellular storage blocks located opposite plots 9-11 within an area of POS. The volume of storage required is approximately 310m3. A Hydrobrake will be fitted to the downstream manhole to restrict flows to 6l/s.

Cellular storage will be maintained by the appointed development management company.

Foul Water

Foul water will drain via gravity into the existing public combined sewer within Harthill Road. Surface water downstream of the Hydrobrake will converge with the foul water and drain via a combined sewer to the outfall. The combined sewer will also receive a combined connection from The Paddock.

All sewers within The Depot Site with the exception of the cellular storage will be offered for adoption with United Utilities.

The Paddock

Surface Water

The northern area of The Paddock will drain via gravity into a series of cellular storage blocks located opposite plot 24 within an area of POS. The volume of storage required is approximately 220m3. A Hydrobrake will be fitted to the downstream manhole to restrict flows to 6l/s.

Again the cellular storage will be maintained by the appointed development management company.

The southern area of The Paddock will drain via gravity to the lowest point of the site adjacent plots 34-36 where it will be attenuated within a series of cellular storage blocks before discharging into a combined pumping station. The combined water will then be pumped approximately 250m into the proposed combined outlet for the northern area of The Paddock. The volume of surface water storage for attenuation is approximately 190m3. An orifice plate will be fitted to the outlet pipe to restrict flows to 5l/s. The attenuation and restriction of surface water flows is prior to discharge to the pumping station.

Foul Water

The northern area of The Paddock will drain via gravity into the proposed combined sewer serving The Depot Site and discharges into existing public combined sewer within Harthill Road. Foul water for the northern area will converge with the surface water downstream of the Hydrobrake.

The southern area of The Paddock will drain via a pumped solution into the proposed combined outlet for the northern area. The pumping station will be located adjacent plots 34-36.

The foul and surface water drainage within the southern area of The Paddock will remain private and maintained by the appointed development management company.

The foul and surface water drainage for the northern area of The Paddock with the exception of the cellular storage will be offered for adoption with United Utilities.

Beechley House

Surface Water

A drainage survey has been undertaken for the area of Beechley House. The results of which identify surface water draining via infiltration. It is proposed that the refurbished buildings will drain via infiltration and a series of soakaways are proposed.

Foul Water

The existing foul drainage network is proposed to be removed and upgraded. It is proposed that the existing outlet pipe into the existing combined public sewer will remain and be utilised to discharge foul flows from this area of the site.

Foul and surface water within Beechley House grounds will be maintained by the appointed development management company.

APPENDIX A

Horthill, Crpop







Revision Date	Amendment			Initials
Development	Harthill	Depot		
Location	Liverpool	•		
Marketing Name				
Drawing Title	DRAINAGE L	_AYOUT Sł	neet 2 of 2	2
Drawing Number	ENG001	-1		
Revision	1	Scale @ A1	1:500	
Drawn By	JJP	Date Started	19.10.16	3
Checked by			Date	
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APPENDIX B





<u>APPENDIX C</u>



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			KEY			(DUASE 1)		
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<u>APPENDIX D</u>

Harthill Estate – Drainage Strategy

			S	OAKAWA	Y TEST	RESULT	S				
		Date of Test:	04-10-16			Hole ID:	S	SA1			
						Test No		1			
		Trial P	it	Length	Width	Depth	Depth fo	or Analysis			
		Dimension	s (m)	1.80	0.70	2.10	().48			
T (n	īme nins) 0.0	Depth of water (m bgl) 1.620	Time (mins)	Depth of water (m bgl)	V _(p75-25) =	Effective sto between effe 75%.	rage volum ective depth	ne in trial pit ns 25% to	=	0.30	m ³
	5.0 10.0 20.0 50.0 90.0	1.650 1.680 1.720 1.820 1.870			a _(p50) =	Initial surface 50% effectiv the base are	e area of tri e depth and ea.	ial pit up to d including	=	2.46	m²
1	20.0 50.0	1.940 1.990			t _(p75-25) =	Time for the 75 % to 25%	water level b effective c	l to fall from lepth.	=	90	min
					Soil infi	Itration rate =	1	V _(p75-25) t _(p75-25) x a _(p50)	₎ x 60		-
					Depth (25%) =	1.98	Depth	ר _(75%) =	1.740	m	
							Soil infilt	ration rate =	2.3E	E-05	m/sec
					Remarks Dry sandst	one, easily br	oken up.				
					Time (mins)					
bgl)	0.00	20 40		60	80	100)				
Water Level (m	1.00										
	2.00					•				•	
BET	TS ASS	SOCIATES DIRAL ENGINEERS			Project:	Harthill D	epot, Liv	erpool		Pro	oject No:

Trial Pit Dimensions (m) Length Width Depth for Analysis Time (mins) Depth of water (m bg) Time (m bg) Depth of water (m bg) Time (m bg) Depth of water (m bg) V [0:5:20] Effective storage volume in trial pit personal storage volume in trial pit personal storage volume in trial pit (m bg) = 0.31 m ² 10.0 1.610 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 50 1.600 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 50.0 1.600 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 50.0 1.600 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 150.0 1.600 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 150.0 1.880 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 150.0 1.880 Image: personal storage volume in trial pit (m bg) = 0.31 m ² 170.0 2.000 Image: personal storage volume in trial pit (m bg) = 0.21 m ² 170.0 2.000 Image: personal storage volume in trial pit (m bg) Trice personal storage volume in trial pit (m bg) = 0.21 m ² 170.0 2.000		Date of Test:	04-10-16			Hole ID:		SA1			
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$						Test No		2			
Dimensions (m) 1.80 0.70 2.10 0.49 Time (mins) Depth of water (mins) Time (mins) Depth of water (mins) Effective storage volume in trial pit (mins) = 0.31 m ³ 0.0 1.610 - <td< td=""><td></td><td>Trial P</td><td>it</td><td>Length</td><td>Width</td><td>Depth</td><td>Depth</td><td>for Analysis</td><td></td><td></td><td></td></td<>		Trial P	it	Length	Width	Depth	Depth	for Analysis			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Dimension	s (m)	1.80	0.70	2.10		0.49			
5.0 Imital surface area of trial pit up to 3 (p50) Imital surf	Time (mins) 0.0	Depth of water (m bgl) 1.610	Time (mins)	Depth of water (m bgl)	Effective storage volume in trial pi $V_{(p75-25)}$ = between effective depths 25% to 75%.				=	0.31	m ³
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	5.0 10.0 15.0 25.0 55.0	1.650 1.690 1.760			a _(p50) =	Initial surfact 50% effectiv the base are	e area of t e depth ar ea.	rial pit up to nd including	=	2.49	m ²
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	85.0 115.0 150.0 170.0	1.820 1.880 1.940 2.000			t _(p75-25) =	Time for the 75 % to 25%	water leve	el to fall from depth.	=	120	min
Image: constraint of the second se					Soil inf	iltration rate =		V _(p75-25) t _(p75-25) x a _{(p50}	₎ x 60		-
Soil infiltration rate = 1.7E-05 m/s Soil infiltration rate = 1.7E-05 m/s Remarks Dry sandstone, easily broken up.						Depth (25%) =	1.9775	Depti	ר _(75%) =	1.733	m
Remarks							Soil infil	tration rate =	1.71	E-05	m/s
Time (mins)					Remarks Dry sands	tone, easily br	oken up.				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u>. </u>			Time (min	s)					
	0.00	20	40	60	80		120		160		1
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		Date of Test:	04-10-16			Hole ID:	SA2	2			
						Test No	1				
		Trial P	it	Length	Width	Depth	Depth for A	nalysis			
		Dimension	is (m)	1.00	0.70	1.45	0.50)			
Tin (mir	ne ns)	Depth of water (m bgl)	Time (mins)	Depth of water (m bgl)	V _(p75-25) =	Effective sto between effe	rage volume ir ective depths 2	n trial pit 25% to	=	0.18	m ³
0. E	.0	0.950				75%.					
5. 25 55 85	0 5.0 5.0	1.000 1.040 1.060			a _(p50) =	Initial surfac 50% effectiv the base are	e area of trial µ re depth and in ea.	bit up to cluding	=	1.55	m ²
115 145 175 205	5.0 5.0 5.0 5.0	1.080 1.100 1.120 1.135			t _(p75-25) =	Time for the 75 % to 25%	water level to 6 effective dep	fall from h.	=	na	min
235 265 295	5.0 5.0 5.0	1.150 1.155 1.160			Soil infil	Soil infiltration rate = $\frac{V_{(p75-25)}}{t_{(p75-25)} \times a_{(p50)} \times a_{(p50)}}$					
						Depth (25%) =	1.325	Depth	1 _(75%) =	1.075	m
							Soil infiltrat	on rate =	#VA	LUE!	m/se
					Remarks						
					Dry sandsto 75% effecti	one, quite der ve depth.	nse. No rate ca	alculated as	s pit faile	ed to di	ain to
		<u> </u>		<u> </u>	Time (mins)	,					
0.	.00 0	50		100	150	200	250		300		350
0.	.20										
(lgq 0.	.40								_		
o. 0.	.60										
0 ater Le	.80										
₿ 1.	.00	•									
1.	.20	•	•	•	• •	•	•	•	•		
1.	.40										

			S	OAKAWA	Y TEST	RESUL	TS				
		Date of Test:	04-10-16			Hole ID	:	SA3			
						Test No)	1			
		Trial P	it	Length	Width	Depth	Depth	for Analysis			
		Dimension	s (m)	1.00	0.70	2.00		0.55			
Tii (mi 0 20	me ins) 0.0	Depth of water (m bgl) 1.450 1.530	Time (mins)	Depth of water (m bgl)	V _(p75-25) =	Effective sto = between eff 75%.	prage volu Tective dep	me in trial pit ths 25% to	=	0.19	m ³
50 80 11 14	0.0 0.0 0.0 0.0	1.610 1.660 1.710 1.750			a _(p50) =	Initial surfact 50% effective the base are	ce area of ve depth a ea.	trial pit up to nd including	=	1.64	m ²
17 20 23	0.0 0.0 0.0	1.790 1.840 1.880			t _(p75-25) =	Time for the 75 % to 25%	e water lev % effective	el to fall from depth.	=	190	min
					Soil inf	iltration rate =		V _(p75-25) t _(p75-25) x a _{(p50}	₎₎ x 60		-
						Depth (25%) =	= 1.8625	Dept	h _(75%) =	1.588	m
							Soil infi	Itration rate =	1.01	E-05	m/sec
					Remarks Dry sandsi	tone, easily b	roken up				
	0		50	100	Time (mins	s)		200			250
(0.00										
	0.40										
el (m bg)	0.60										
iter Lev	1.00										
M.	1.40]
1	1.60	•		•	•	•					
2	2.00							•		•	
BETT	S AS				Project:	Harthill D)epot, Li	verpool		Pro	oject No:

			S	OAKAWA	Y TEST	RESULT	S				
		Date of Test:			Hole ID:		SA3				
						Test No		2			
		Trial Pit		Length	Width	Depth	Depth	for Analysis			
		Dimensions (m)		1.00	0.70	2.00		0.58			
											
ר (r	Time mins)	e Depth of water Time s) (m bgl) (mins)		Depth of water (m bgl)	Effective storage volume in trial pit $V_{(p75-25)}$ = between effective depths 25% to					0.20	m ³
-	0.0 10.0	1.420 1.460	75%.								
20.0 30.0 60.0 90.0		1.470 1.490 1.540			a _(p50) =	Initial surface area of trial pit up to = 50% effective depth and including			=	1.69	m ²
		1.580			the base area.						
1	120.0 150.0 180.0	1.620 1.660 1.700			t _(p75-25) =	$T_{75-25} = \frac{1}{75\%}$ Time for the water level to fall from 75% to 25% effective depth.			=	230	min
22	240.0 240.0 270.0	1.740 1.780 1.820 1.860			Soil infi	V _(p75-25)	" x 60		_		
	,00.0	1.000			(p/5-25) X X (jj x 00		
						Depth (25%) =	1.855	Dept	h _(75%) =	1.565	m
<u> </u>							Soil infi	tration rate =	8.7	E-06	m/sec
					Remarks	arks andstone, easily broken up. 75% time extrap					
					Dry sandst						
					Time (mins)					
	0	0 50 100				200	2	50	300		350
	0.20										
Î	0.40										
(m bg	0.60										
r Level	1.00										
Wate	1.20										
	1.40	* * * *	•								
	1.80				+ +	•	•	+			
	2.00										
Project: Harthill Depot, Liverpool											ject No: